

## DECORATED GLASS-CERAMIC PLATE AND CORRESPONDING METHOD OF DECORATION

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The invention relates to a decorated glass-ceramic plate, suitable in particular as a cooktop, comprising a glass-ceramic plate having a low coefficient of thermal expansion between  $+15 \times 10^{-7}$  K $^{-1}$  (20-700 DEG C.) and a decoration on the surface of said plate. Characteristically, said decoration comprises a vitrified glass frit containing 10 to 35% by weight of pigments and said decorated glass-ceramic cooktop has a modulus of rupture of at least 120 MPa. The invention also relates to a method of decorating glass-ceramic plates and to an enamel which is useful in particular for implementing said method.

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**(54) DECORATED GLASS-CERAMIC PLATE AND CORRESPONDING METHOD OF DECORATION**

**DEKORIERTE GLASKERAMISCHE SCHEIBE UND VERFAHREN ZUR DEKORATION**

**PLAQUE VITRO-CERAMIQUE DECOREE ET PROCEDE DE DECORATION ASSOCIE**

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**Description**

[0001] The present invention relates to a decorated glass-ceramic plate as well as to a method of obtaining such a plate, i.e. a method of decorating a glass-ceramic plate. Such plates are especially used as cooktops.

[0002] Another object of the present invention is an enamel, useful in particular in the implementation of said decoration method.

[0003] The cooking surface defined by a glass-ceramic plate, when it is used as a cooktop, must withstand not only the elevated temperatures employed for cooking without softening or distorting, but also it must withstand large differences in temperature which result from the fact that only one or more parts of the plate are heated. This has led to the use, in this field, of glass-ceramic plates having a coefficient of thermal expansion of zero or near-zero, i.e. generally equal to  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$ , and preferably zero.

[0004] Glass-ceramics having these characteristics are well known and are widely described in the literature. United States Patent No. 5,070,045 (Comte et al.) describes such glass-ceramics the predominant crystal phase of which is a beta-quartz crystal phase. According to the present invention, decorative materials have been developed which are intended to be used especially, but not exclusively, with such glass-ceramics. It is as such that they can also be used with other low expansion glass-ceramics such as those described in the French patent application No. 97 09912.

[0005] Glass-ceramic plates have proved to be extremely satisfactory from the functional point of view as cooktops, but for aesthetic reasons, it was found that it was desirable to decorate the upper surface of said plates.

[0006] Enamelling is the decoration method which has proved to be the easiest to implement and which, consequently, is the most generally used. The main points of this technique, which are familiar to the person skilled in the art, have been summarised in the introductory part of the French patent application FR-A-2 701 473.

[0007] The initial problem which arises is that of the compatibility of the decorations with the glass-ceramics. In fact, there generally exists a difference in the thermal expansion between the glass-ceramic and the decoration. This difference in expansion of course lowers the mechanical strength of said plate comprising said decoration.

[0008] Glass-ceramics have a more than satisfactory inherent mechanical strength, the modulus of rupture (MOR) of the materials actually used being about 180 MPa. However, while the mechanical strength of the actual decorated plates is still adequate, it is significantly reduced and it has revealed to be desirable to obtain higher values, particularly if it has revealed to be desirable to obtain decorated glass-ceramic plates having a modulus of rupture (MOR) of at least 120 MPa, preferably of at least about 130 MPa.

[0009] Apart from the aesthetic aspect and the problem of the mechanical strength of the decorated plate, a cooktop must also resist staining due to food, it must be easy to clean and must have a smooth surface in order to prevent marks due to contact with metal utensils. These requirements severely limit the potential decoration materials.

[0010] For example, a logical candidate was a glass frit that crystallises to produce a low expansion crystal phase, especially a beta-quartz crystal phase. The coatings constituted by these crystallised frits have a very satisfactory modulus of rupture (MOR) but their surface properties are mediocre since the crystals give rise to a surface roughness which is unacceptable, as regards marks left by metallic utensils, and possibilities of easy cleaning.

[0011] The United States Patent No. 5,326,728 (Boury et al.), which corresponds to the French patent application FR-A-2 701 473, describes enamels used in the production of decorative materials. Although these materials have proved to be satisfactory, efforts have been made to produce further improved decorative materials. In particular, these efforts have been directed at obtaining a coefficient of thermal expansion of the decoration which is more compatible with that of the plate ; this being in order to obtain a greater mechanical strength of the decorated article, and this is indicated by a higher modulus of rupture (MOR).

[0012] Thus, an object of the present invention is to provide a glass-ceramic plate which comprises an improved decoration and which has a modulus of rupture (MOR) of greater than 120 MPa whilst at the same time meets the various other requirements of such an article used as a cooktop (requirements recalled above), which has a great flexibility in decoration, which has an improved decoration comprising a mixture of a glass frit with pigments capable of providing a desired decorative effect; as well as to provide a decorative material (an enamel) which can be fired to produce an adherent decoration, especially during the firing of a glass plate to convert the glass into a glass-ceramic; as well as to provide a method of decorating such a glass-ceramic plate.

[0013] The present invention does in fact relate to a decorated glass-ceramic plate comprising a glass-ceramic plate having a low coefficient of thermal expansion between  $\pm 15 \times 10^{-7} \text{ K}^{-1}$  (20-700°C), preferably near-zero (i.e. equal to  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$  (20 - 700°C)), and a decoration on the surface of said plate, said decoration comprising a vitrified glass frit containing 10 to 35 % by weight of pigments (for 90 to 65 % by weight of frit), and said decorated glass-ceramic plate having a modulus of rupture (MOR) of at least 120 MPa. The glass frit employed for the decoration according to the invention has a coefficient of thermal expansion of  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300°C), preferably of at most 35  $\times 10^{-7} \text{ K}^{-1}$ , and a softening point of at least 750°C, preferably of at least 775°C. The composition of said glass, calculated in weight % of oxides, consists, essentially, of 70-82 %  $\text{SiO}_2$ , 12-18 %  $\text{B}_2\text{O}_3$ , 1-3 %  $\text{Al}_2\text{O}_3$ , at most 5 %  $\text{Na}_2\text{O} + \text{K}_2\text{O}$  and at most 1.2 % of at least one fining agent.

[0014] Preferably, the decorated glass-ceramic plate is constituted by a glass-ceramic the predominant crystal phase of which is a solid solution of beta-quartz and which advantageously has a coefficient of thermal expansion of  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$  ( $20 - 700^\circ\text{C}$ ).

[0015] The present invention also relates to a method of decorating a glass-ceramic plate, especially for generating a decorated cooktop for a cooking appliance, said glass-ceramic plate having a low coefficient of thermal expansion (see above), preferably near-zero (see above), said method comprising :

- producing a mixture of 65 to 90 % by weight of a glass frit and of 10 to 35 % by weight of pigments ; said glass frit having a coefficient of thermal expansion of  $30-40 \times 10^{-7} \text{ K}^{-1}$  ( $0-300^\circ\text{C}$ ) (preferably of  $30-35 \times 10^{-7} \text{ K}^{-1}$  ( $10-300^\circ\text{C}$ )) and a softening point of at least  $750^\circ\text{C}$  (preferably of at least  $775^\circ\text{C}$ ), and the composition of said glass frit, calculated in weight % of oxides, consists, essentially, of 70-82 %  $\text{SiO}_2$ , 12-18 %  $\text{B}_2\text{O}_3$ , 1-3 %  $\text{Al}_2\text{O}_3$ , at most 5 %  $\text{Na}_2\text{O} + \text{K}_2\text{O}$  and at most 1.2 % of at least one fining agent
- applying said glass frit/pigments mixture onto the surface of a glass-ceramic plate or onto the surface of a glass-ceramic precursor glass plate ;
- firing said plate coated with said glass frit/pigments mixture, to optionally transform said glass plate into a glass-ceramic plate, to vitrify the glass frit in the frit/pigments mixture, to obtain an adherence of the generated decoration with the glass-ceramic; and
- cooling said fired plate in order to obtain a decorated glass-ceramic plate having a modulus of rupture of at least 120 MPa.

[0016] The present Invention is derived from research carried out to produce an improved decorative material for a glass-ceramic plate. In particular, a material was sought which was suitable for glass-ceramic plates the predominant crystal phase of which is a beta-quartz crystal phase and which has a coefficient of thermal expansion of near to zero, preferably of  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$  ( $20 - 700^\circ\text{C}$ ). The decorative material according to the Invention meets this requirement but is not limited to such an application and can be used effectively on other glass-ceramics having a low coefficient of thermal expansion, i.e. situated in the range of  $0 \pm 15 \times 10^{-7} \text{ K}^{-1}$  ( $20-700^\circ\text{C}$ ).

[0017] The decorative materials used according to the prior art generally comprise pigments dispersed in a glass frit. Said pigments confer to said material its colour and its opacity whereas the glass ensures their mutual binding and their adherence with the glass-ceramic. A glass which is suitable as a frit was described by the Applicant in the United States Patent No. 5,326,728 and consists of a boroaluminosilicate glass which has a coefficient of thermal expansion of about  $55 \times 10^{-7} \text{ K}^{-1}$  ( $0-300^\circ\text{C}$ ) and a softening point of about  $675^\circ\text{C}$ . (see Composition A of Table II below).

[0018] In the course of the research to produce a decorated glass-ceramic having a higher mechanical strength, two factors became apparent which were particularly important for increasing the mechanical strength of a decorated glass-ceramic plate. The first related to the lowering of the coefficient of thermal expansion of the glass frit, and this can be accomplished by means of a frit that can crystallise. However, as indicated above, this approach revealed to be unfruitful due to the fact that the rough surface produced by the crystals is sensitive to marks made by metal utensils and is difficult to clean, and this constitutes an important drawback in the field of the preparation of food. This lack of success led to further studies on glass frits which do not crystallise. The other important factor which was discovered, in a non-obvious way, is that it is important to limit the ionic diffusion which takes place across the interface between the decoration and the glass-ceramic substrate.

[0019] The phenomenon of alkali metal ion migration is well known and it was noted that it was not possible to eliminate the presence of the alkali metal ions from the frit without creating other problems despite the presence of said ions being limited. It then appeared important to employ a frit of glass of high viscosity ; this being evidenced by a high softening point. In fact, this apparently inhibits the tendency of the alkali metal ions to migrate during heat treatments.

[0020] The decorative material according to the present Invention essentially consists of 10 to 35% by weight of pigments dispersed in 65 to 90% by weight of glass frit. At least 10% by weight of pigments is necessary to obtain a suitable effect and it is possible to incorporate up to about 35% by weight of pigments. Generally, in order to obtain the decorative effect anticipated, it is not necessary to include more than about 20% by weight of such pigments.

[0021] It is possible to use any commercial pigment individually or in combination. The particular pigment or pigments which are employed depend upon the opacity and particular colour desired, or upon another decorative effect desired.

[0022] Table I below shows two examples of individual pigments and an example of a combination that can be used. In each case, the pigments are mixed in an amount of 15 % by weight with 85 % by weight of a glass frit defined below. Table I identifies the pigments by their source, their main constitutive elements and the colour of the coating after firing.

TABLE I

| MIXTURE | PIGMENTS   | MAIN ELEMENTS                       | COLOUR |
|---------|--|-------------------------------------|--------|
| 1       | -  | TiO <sub>2</sub>                    | White  |
| 2       | FA 9150 (Bayer)                                    | Tl, Sb, V                           | Brown  |
| 3       | X928 (CERDEC)<br>B768 (CERDEC)<br>EV 1092 (CERDEC) | Co, Al<br>Cr, Co, Ni, Fe,<br>Co, Cr | Black  |

[0023] The glass frit employed for the decoration according to the invention has a coefficient of thermal expansion of  $30-40 \times 10^{-7} \text{ K}^{-1}$  ( $0-300^\circ \text{ C}$ ), preferably of at most  $35 \times 10^{-7} \text{ K}^{-1}$ , and a softening point of at least  $750^\circ \text{ C}$ ., preferably of at least  $775^\circ \text{ C}$ . At the softening point, the viscosity of a glass is  $10^6.5 \text{ Pa.s}$  ( $10^{7.5}$  poises).

[0024] Said included glass is generally a soda potash borosilicate. In fact, it was observed that such glasses possess the characteristics set forth above.

[0025] The composition of said included glass, calculated in weight % of oxides, consists, essentially, of 70-82% SiO<sub>2</sub>, 12-18% B<sub>2</sub>O<sub>3</sub>, 1-3% Al<sub>2</sub>O<sub>3</sub>, at most 5% Na<sub>2</sub>O + K<sub>2</sub>O and at most 1.2% of at least one fining agent. According to a particularly preferred variant, the composition essentially consists of 76-81% SiO<sub>2</sub>, 14-15.5% B<sub>2</sub>O<sub>3</sub>, 2-2.7% Al<sub>2</sub>O<sub>3</sub>, 2.3-3.2% Na<sub>2</sub>O, 1-1.5% K<sub>2</sub>O, 0-1% As<sub>2</sub>O<sub>3</sub> + Sb<sub>2</sub>O<sub>3</sub> (+ meaning « and/or »).

[0026] Table II below shows a comparison of the composition of a glass frit from the United States Patent No. 5,326,728 cited above (A) with a composition of a preferred glass frit according to the present invention (B). The compositions are indicated in weight % of the glass batch.

TABLE II

|  | A                   | B                   |
|--|---------------------|---------------------|
| SiO <sub>2</sub>   | 41.8                | 78.3                |
| B <sub>2</sub> O <sub>3</sub>                                    | 27.4                | 14.75               |
| Al <sub>2</sub> O <sub>3</sub>                                   | 18.7                | 2.25                |
| Li <sub>2</sub> O  | 2.6                 | -                   |
| Na <sub>2</sub> O  | 0.8                 | 2.6                 |
| K <sub>2</sub> O   | 3.4                 | 1.25                |
| CaO  | 2.8                 | -                   |
| ZrO <sub>2</sub>   | 2.5                 | -                   |
| As <sub>2</sub> O <sub>3</sub>                                   | -                   | 0.85                |
| Softening point ( $^\circ\text{C}$ )                             | 676                 | 780                 |
| Coefficient of thermal expansion ( $\text{K}^{-1}$ ( $0-300$ ))) | $55 \times 10^{-7}$ | $34 \times 10^{-7}$ |

[0027] A glass frit is prepared by mixing a batch of suitable starting materials and melting it at about  $1650^\circ \text{ C}$ . for about six hours. The molten glass is poured into water wherein it fractures into particles which are dried and ground to a powder having an average particle size of less than about  $6 \mu\text{m}$ .

[0028] The pigments are then added which are mixed with the powdered glass frit. The nature of the pigments, and their amounts, depend upon the desired colour and opacity for a particular application. The coating mixture contains at least 10% by weight of pigments, and may contain up to 35% (see above). The balance is constituted by the glass frit. A mixture of 15% pigments and 85% glass frit has proved satisfactory for most of the applications. This mixture should be homogeneous, but no special mixing procedure is required.

[0029] The application of a slip or paste by screen printing, which gives a thin uniform coating, constitutes a suitable means of applying said mixture onto a glass-ceramic plate. For such an application, an organic vehicle is added, typically in an amount of 30 - 50% by weight of the total weight of the slip. The amount of vehicle depends upon the ultimate thickness desired. If a design is desired, the screen printing screen can be prepared in the form of a mask in a known manner.

[0030] According to the present invention, it is advantageous that the decorative material can be applied onto the surface of the glass plate which constitutes a precursor for the glass-ceramic plate. After drying, the material on the glass plate can be heat treated according to a ceramming cycle that converts the glass into a glass-ceramic. At the same time, the glass frit, present in the decorating material, softens and bonds to the pigments and onto the surface of the glass-ceramic.

[0031] As described in the United States Patent No. 5,070,045, already cited, a suitable ceramming schedule is as follows:

- a temperature increase at a rate of 50 - 80 °C./min up to the nucleation range, generally located close to the transformation range of the glass,
- a temperature increase in the range of nucleation (670-800° C.) in about 15 - 25 min,
- a temperature increase up to the crystallisation temperature (900-960° C.) in about 15 - 30 min,
- maintaining the crystallisation temperature for 10 - 25 min, and
- rapid cooling to ambient temperature.

[0032] Other types of heat treatment or firing may be used in order to ensure the desired effects : ceramming the glass plate + vitrification of the pigment-loaded frit + adhesion of said loaded frit onto the cerammed glass plate. Thus, the decorative material can be applied onto the crude glass plates as described in the French patent application No. 97 09912 and the ceramming cycles, as described in said French patent application No. 97 09912, can be implemented in order to obtain decorated glass-ceramic plates of the invention based on the glass-ceramic plates according to the French patent application No. 97 09912. The maximum temperatures attained during said ceramming cycles may attain values as high as 1070° C. In said French patent application No. 97 09912, ceramming cycles are also described which comprise several successive cycles. In such cases, it is preferred to apply the glass frit/pigments mixture (precursor of the desired decoration) before the last of said successive cycles such that said mixture undergoes one sole heat treatment only.

[0033] Hence, it is understood that the expression « glass-ceramic precursor glass plate », as used in the present description and the annexed claims, incorporates both the crude glass plate as well as the glass plate undergoing ceramming.

[0034] For some applications, it may be desirable, or even necessary, to apply the material onto the already cerammed glass-ceramic plate. In this case, the coating can be applied in the same manner as in the case of a precursor glass plate, but directly onto the glass-ceramic plate. This double firing procedure (1<sup>o</sup> ceramming; 2<sup>o</sup> treatment of the glass frit/pigments mixture) may be desirable for adjusting each firing cycle. In this case, the material situated on the glass-ceramic may be fired for about 15 minutes at a temperature in the range of 920 - 960° C.

[0035] Another object of the present invention is the enamel used for the implementation of the decorating method described above, used for obtaining the decorated glass-ceramic plates of the invention. Said enamel is novel *per se*, and constitutes another object of the present invention. Characteristically, the enamel comprises 10 to 35% by weight of pigments in 65 to 90% by weight of a specific glass frit. Said glass frit has a coefficient of thermal expansion of 30 - 40 x 10<sup>-7</sup> K<sup>-1</sup> (0 - 300° C.), preferably of 30 - 35 x 10<sup>-7</sup> K<sup>-1</sup> (0 - 300° C.) and a softening point of at least 750° C., preferably of at least 775° C. and the composition of said glass frit, calculated in weight % of oxides, essentially consists of 70-82% SiO<sub>2</sub>, 12-18% B<sub>2</sub>O<sub>3</sub>, 1-3% Al<sub>2</sub>O<sub>3</sub>, at most 5% Na<sub>2</sub>O + K<sub>2</sub>O and at most 1.2 % of at least one fining agent. Particularly preferably, said composition essentially consists of 78-81% SiO<sub>2</sub>, 14-15.5% B<sub>2</sub>O<sub>3</sub>, 2-2.7% Al<sub>2</sub>O<sub>3</sub>, 2.3-3.2% Na<sub>2</sub>O, 1-1.5% K<sub>2</sub>O and 0-1 % As<sub>2</sub>O<sub>3</sub> + Sb<sub>2</sub>O<sub>3</sub>.

[0036] The invention is illustrated by two Examples 1 and 2 below, which are to be considered in parallel with the Comparative Example 3.

[0037] Decorated glass-ceramic plates were prepared according to the invention with the glass frit B the composition and characteristics of which are given in Table II above ; a prior art decorated glass-ceramic plate was prepared with the glass frit A the composition and characteristics of which are also given in Table II above.

[0038] The respective contents of frit and pigments in the mixtures prepared are indicated in Table III below (contents expressed in % by weight). The properties of the plates obtained, decorated with said mixtures, are also indicated.

[0039] The conditions under which said decorated plates are obtained, and the methods of evaluation of their properties, are then specified.

TABLE III

| Examples                           | 1   | 2    | 3  |
|------------------------------------|-----|------|----|
| Frit                               | B   | B    | A  |
| % frit                             | 85  | 85   | 70 |
| % pigments                         | 15  | 15   | 30 |
| Plate properties                   |     |      |    |
| Modulus of rupture<br>(MOR in MPa) | 150 | >120 | 70 |

TABLE III (continued)

| Examples                | 1   | 2   | 3   |
|-------------------------|-----|-----|-----|
| <b>Plate properties</b> |     |     |     |
| . Resist metal marks    | yes | yes | yes |
| . Easily cleanable      | yes | yes | yes |

[0040] The plates of Examples 1 and 2 were therefore decorated with mixtures containing the glass frit B, while the plate of the Comparative Example 3 was decorated with a mixture containing the glass frit A.

[0041] Said mixtures were obtained with the same pigments (pigment mixture 3 of the Table I). The mixtures were constituted with a vehicle in order to be applicable on the plates by screen printing.

[0042] For Examples 1 and 3, the mixture was applied by screen printing onto the upper surface of a glass plate precursor for a glass-ceramic plate having a coefficient of thermal expansion of zero. The glass plate was then dried and heat treated according to the ceramming cycle for the glass which was a cycle of 1 hour with a maximum temperature of 925° C., which was maintained for 15 minutes. During this heating cycle, the glass plate was transformed into a glass-ceramic and the decorative mixture had become an adherent vitrified layer the thickness of which was about 3 µm.

[0043] For Example 2, the mixture was applied onto the upper surface of a glass plate precursor for a glass-ceramic plate which had a coefficient of thermal expansion equal to  $10 \times 10^{-7} \text{ K}^{-1}$ . The ceramming cycle was a cycle of 2 h, with a maximum temperature of 1070° C. which was maintained for 30 min. The decoration obtained had itself a thickness of 3µm as well.

[0044] The modulus of rupture (MOR) was measured by means of a 3 points flexion setting, the decorated surface being in extension. According to the invention, a modulus of rupture of at least 120 MPa is specified and a value of at least 130 MPa is preferred.

[0045] The cleanability was evaluated in the following manner: a mixture of meat, egg, milk, flour, gruyère cheese, tapioca and tomato purée was placed between a saucepan full of water and the decorated zone of the cooktop. The whole was then heated for 10 minutes such that the mixture burns and sticks to the cooktop. The cleanability and the aspect of the decoration after cleaning are then evaluated.

[0046] The formation of marks by metals was evaluated by marking the decorated surface with a metallic piece. The result is satisfactory if only light marks are observed, and it is possible to remove them with a commercial product sold for cleaning cooktops.

### Claims

1. A decorated glass-ceramic plate, particularly suitable as a cooktop, comprising a glass-ceramic plate having a low coefficient of thermal expansion between  $\pm 15 \times 10^{-7} \text{ K}^{-1}$  (20-700° C) and a decoration on the surface of said plate, characterised in that said decoration comprises a vitrified glass frit:

- said glass frit having a coefficient of thermal expansion of  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300° C), preferably of  $30-35 \times 10^{-7} \text{ K}^{-1}$  (0-300° C) and a softening point of at least 750°C, preferably of at least 775°C;
- the composition of said glass frit, calculated in weight % of oxides, essentially consisting of 70-82 %  $\text{SiO}_2$ , 12-18 %  $\text{B}_2\text{O}_3$ , 1-3 %  $\text{Al}_2\text{O}_3$ , at most 5 %  $\text{Na}_2\text{O} + \text{K}_2\text{O}$  and at most 1.2 % of at least one fining agent; and
- said glass frit containing 10 to 35 % by weight of pigments;

and in that said decorated glass-ceramic plate has a modulus of rupture of at least 120 MPa.

2. The decorated glass-ceramic plate according to claim 1, characterised in that the glass which constitutes said frit is a soda potash borosilicate.

3. The decorated glass-ceramic plate according to one of claims 1 or 2, characterised in that the composition of said glass frit essentially consists of 76-81 %  $\text{SiO}_2$ , 14-15.5 %  $\text{B}_2\text{O}_3$ , 2-2.7 %  $\text{Al}_2\text{O}_3$ , 2.3-3.2 %  $\text{Na}_2\text{O}$ , 1-1.5 %  $\text{K}_2\text{O}$  and 0-1 %  $\text{As}_2\text{O}_3 + \text{Sb}_2\text{O}_3$ .

4. The decorated glass-ceramic plate according to any one of claims 1 to 3, characterised in that said glass-ceramic plate has a coefficient of thermal expansion in the range of  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$  (20-700° C).

5. A method of decorating a glass-ceramic plate, said plate having a low coefficient of thermal expansion between  $\pm 15 \times 10^{-7} \text{ K}^{-1}$  (20-700°C), characterised in that it comprises :

producing a mixture of 65 to 90 % by weight of a glass frit and of 10 to 35 % by weight of pigments, said glass frit having a coefficient of thermal expansion of  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300°C), preferably of  $30-35 \times 10^{-7} \text{ K}^{-1}$  (0-300°C) and a softening point of at least 750°C, preferably of at least 775°C and the composition of said glass frit, calculated in weight % of oxides, essentially consisting of 70-82 %  $\text{SiO}_2$ , 12-18 %  $\text{B}_2\text{O}_3$ , 1-3 %  $\text{Al}_2\text{O}_3$ , at most 5 %  $\text{Na}_2\text{O} + \text{K}_2\text{O}$  and at most 1.2 % of at least one fining agent;

10 applying said glass frit/pigments mixture onto the surface of a glass-ceramic plate or onto the surface of a glass-ceramic precursor glass plate;

firing said plate coated with said glass frit/pigments mixture, to optionally transform said glass plate into a glass-ceramic plate, to vitrify the glass frit in the frit/pigments mixture, and to provide an adherence of the generated decoration with the glass-ceramic ; and

15 cooling said fired plate to obtain a decorated glass-ceramic plate having a modulus of rupture of at least 120 MPa.

6. The method according to claim 5, characterised in that it comprises applying said glass frit/pigments mixture onto the surface of a glass-ceramic plate and then heat treating said glass frit/ pigments mixture for about 15 min at a temperature in the range of 920-960°C.

20 7. The method according to one of claims 5 or 6, characterised in that it comprises applying said glass frit/pigments mixture onto the surface of a glass-ceramic plate having a coefficient of thermal expansion in the range of  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$  (20-700°C).

25 8. The method according to claim 5, characterised in that it comprises applying said glass frit/pigments mixture onto the surface of a glass-ceramic precursor glass plate and then heat treating said precursor glass plate and said glass frit/pigments mixture applied thereon, according to the following schedule :

30 a temperature increase at a rate of 50-80°C/min up to the nucleation range, generally located close to the transformation range of the glass,  
a temperature increase in the range of nucleation (670-800°C) in about 15-25 min,  
a temperature increase up to the crystallisation temperature (900-960°C) in about 15-30 min,  
maintaining the crystallisation temperature for 10-25 min, and  
rapid cooling to ambient temperature.

35 9. An enamel, useful in particular for implementing the method according to any one of claims 5 to 8, characterised in that it comprises 10 to 35 % by weight of pigments and 65 to 90 % by weight of a glass frit having a coefficient of thermal expansion of  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300°C), preferably of  $30-35 \times 10^{-7} \text{ K}^{-1}$  (0-300°C) and a softening point of at least 750°C, preferably of at least 775°C ; the composition of said glass frit, calculated in weight % of oxides, essentially consisting of 70-82 %  $\text{SiO}_2$ , 12-18 %  $\text{B}_2\text{O}_3$ , 1-3 %  $\text{Al}_2\text{O}_3$ , at most 5 %  $\text{Na}_2\text{O} + \text{K}_2\text{O}$  and at most 1.2 % of at least one fining agent.

40 10. The enamel according to claim 9, characterized in that the composition of said glass frit, calculated in weight % of oxides, essentially consists of 76-81 %  $\text{SiO}_2$ , 14-15.5  $\text{B}_2\text{O}_3$ , 2-2.7 %  $\text{Al}_2\text{O}_3$ , 2.3-3.2 %  $\text{Na}_2\text{O}$ , 1-1.5 %  $\text{K}_2\text{O}$  and 0-1 %  $\text{As}_2\text{O}_3 + \text{Sb}_2\text{O}_3$ .

#### Patentansprüche

45 1. Dekorierte Glaskeramikplatte, die insbesondere als Herd-Kochplatte geeignet ist, die umfasst eine Glaskeramikplatte mit einem niedrigen Wärmeausdehnungskoeffizienten zwischen  $\pm 15 \times 10^{-7} \text{ K}^{-1}$  (20 - 700 °C) und eine Dekoration auf der Oberfläche dieser Platte, dadurch gekennzeichnet, dass die Dekoration umfasst eine vitrifierte Glasfritte:

50 - die einen Wärmeausdehnungskoeffizienten von 30 bis  $40 \times 10^{-7} \text{ K}^{-1}$  (0 - 300 °C), vorzugsweise von 30 bis  $35 \times 10^{-7} \text{ K}^{-1}$  (0 - 300 °C), und einen Erweichungspunkt von mindestens 750 °C, vorzugsweise von mindestens 775 °C, aufweist;  
- deren Zusammensetzung, berechnet in Gew.-% Oxiden, im wesentlichen besteht aus 70 bis 82 %  $\text{SiO}_2$ , 12

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bis 18 %  $B_2O_3$ , 1 bis 3 %  $Al_2O_3$ , höchstens 5 %  $Na_2O + K_2O$  und höchstens 1,2 % mindestens eines Läuterungsmittels, und

- die 10 bis 35 Gew.-% Pigmente enthält; und

5 dass die dekorierte Glaskeramikplatte einen Bruchmodul (Biegefestigkeit) von mindestens 120 MPa aufweist.

2 Dekorierte Glaskeramikplatte nach Anspruch 1, dadurch gekennzeichnet, dass das Glas, das die Fritte aufbaut, ein Soda-Pottasche-Borsilikat ist.

10 3. Dekorierte Glaskeramikplatte nach einem der Ansprüche 1 oder 2, dadurch gekennzeichnet, dass die Zusammensetzung der Glasfritte im wesentlichen besteht aus 76 bis 81 %  $SiO_2$ , 14 bis 15,5 %  $B_2O_3$ , 2 bis 2,7 %  $Al_2O_3$ , 2,3 bis 3,2 %  $Na_2O$ , 1 bis 1,5 %  $K_2O$  und 0 bis 1 %  $As_2O_3 + Sb_2O_3$ .

15 4. Dekorierte Glaskeramikplatte nach einem der Ansprüche 1 bis 3, dadurch gekennzeichnet, dass sie einen Wärmeausdehnungskoeffizienten in dem Bereich von  $0 \pm 3 \times 10^{-7} K^{-1}$  (20 - 700 °C) aufweist.

5. Verfahren zum Dekorieren einer Glaskeramikplatte, die einen niedrigen Wärmeausdehnungskoeffizienten zwischen  $\pm 15 \times 10^{-7} K^{-1}$  (20 - 700 °C) aufweist, dadurch gekennzeichnet, dass es umfasst:

20 das Herstellen einer Mischung aus 65 bis 90 Gew.-% einer Glasfritte und 10 bis 35 Gew.-% Pigmenten, wobei die Glasfritte einen Wärmeausdehnungskoeffizienten von 30 bis  $40 \times 10^{-7} K^{-1}$  (0 - 300 °C), vorzugsweise von 30 bis  $35 \times 10^{-7} K^{-1}$  (0 - 300 °C), und einen Erweichungspunkt von mindestens 750 °C, vorzugsweise von mindestens 775 °C, sowie eine Zusammensetzung, berechnet in Gew.-% Oxiden, aufweist, die im wesentlichen besteht aus 70 bis 82 %  $SiO_2$ , 12 bis 18 %  $B_2O_3$ , 1 bis 3 %  $Al_2O_3$ , höchstens 5 %  $Na_2O + K_2O$  und höchstens 1,2 % mindestens eines Läuterungsmittels;

25 das Aufbringen dieser Mischung aus der Glasfritte und Pigmenten auf die Oberfläche einer Glaskeramikplatte oder auf die Oberfläche einer Glaskeramik-Vorläufer-Glasplatte;

30 das Brennen der mit der Glasfritte/Pigmentmischung beschichteten Platte, um gegebenenfalls die Glasplatte in eine Glaskeramikplatte zu überführen, um die Glasfritte in der Glasfritte/Pigmentmischung zu vitrifizieren und eine Haftung der erzeugten Dekoration an der Glaskeramik zu bewirken; und

35 das Abkühlen der gebrannten Platte zur Herstellung einer dekorierten Glaskeramikplatte, die einen Bruchmodul (Biegefestigkeit) von mindestens 120 MPa aufweist.

6. Verfahren nach Anspruch 5, dadurch gekennzeichnet, dass es umfasst das Aufbringen der Glasfritte/Pigmentmischung auf die Oberfläche einer Glaskeramikplatte und das anschließende etwa 15-minütige Wärmebehandeln der Glasfritte/Pigmentmischung bei einer Temperatur in dem Bereich von 920 bis 960 °C.

7. Verfahren nach einem der Ansprüche 5 oder 6, dadurch gekennzeichnet, dass es umfasst das Aufbringen der Glasfritte/Pigmentmischung auf die Oberfläche einer Glaskeramikplatte, die einen Wärmeausdehnungskoeffizienten in dem Bereich von  $0 \pm 3 \times 10^{-7} K^{-1}$  (20 - 700 °C) aufweist.

40 8. Verfahren nach Anspruch 5, dadurch gekennzeichnet, dass es umfasst das Aufbringen der Glasfritte/Pigmentmischung auf die Oberfläche einer Glaskeramik-Vorläufer-Glasplatte und das anschließende Wärmebehandeln dieser Vorläufer-Glasplatte und der darauf aufgebrachten Glasfritte/Pigmentmischung nach dem folgenden Programm:

45 Erhöhen der Temperatur mit einer Geschwindigkeit von 50 bis 80 °C/min bis auf den Kristallisationskeimbildungsbereich, der im allgemeinen nahe bei dem Glasumwandlungsbereich liegt,

50 Erhöhen der Temperatur innerhalb von etwa 15 bis 25 min in dem Kristallisationskeimbildungsbereich (670 - 800 °C),

Erhöhen der Temperatur innerhalb von etwa 15 bis 30 min bis auf die Kristallisationstemperatur (900 - 960 °C), 10 bis 25-minütiges Halten der Kristallisationstemperatur und

55 schnelles Abkühlen auf Umgebungstemperatur.

9. Email (Glasur), die insbesondere verwendbar ist zur Durchführung des Verfahrens nach einem der Ansprüche 5 bis 8, dadurch gekennzeichnet, dass sie umfasst 10 bis 35 Gew.-% Pigmente und 65 bis 90 Gew.-% einer Glasfritte, die einen Wärmeausdehnungskoeffizienten von 30 bis  $40 \times 10^{-7} K^{-1}$  (0 - 300 °C), vorzugsweise von 30

bis  $35 \times 10^{-7} \text{ K}^{-1}$  (0 - 300 °C), einen Erweichungspunkt von mindestens 750 °C, vorzugsweise von mindestens 775 °C; und eine Zusammensetzung aufweist, die, berechnet in Gew.-% Oxiden, im wesentlichen besteht aus 70 bis 82 % SiO<sub>2</sub>, 12 bis 18 % B<sub>2</sub>O<sub>3</sub>, 1 bis 3 % Al<sub>2</sub>O<sub>3</sub>, höchstens 5 % Na<sub>2</sub>O + K<sub>2</sub>O und höchstens 1,2 % mindestens eines Läuterungsmittels.

5            10. Email (Glasur) nach Anspruch 9, dadurch gekennzeichnet, dass die Zusammensetzung der Glasfritte, berechnet in Gew.-% Oxiden, im wesentlichen besteht aus 76 bis 81 % SiO<sub>2</sub>, 14 bis 15,5 % B<sub>2</sub>O<sub>3</sub>, 2 bis 2,7 % Al<sub>2</sub>O<sub>3</sub>, 2,3 bis 3,2 % Na<sub>2</sub>O, 1 bis 1,5 % K<sub>2</sub>O und 0 bis 1 % As<sub>2</sub>O<sub>3</sub> + Sb<sub>2</sub>O<sub>3</sub>.

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#### Revendications

15            1. Plaque de vitrocéramique décorée, convenant notamment à titre de plaque de cuisson, comprenant une plaque de vitrocéramique ayant un faible coefficient de dilatation thermique compris entre  $\pm 15 \times 10^{-7} \text{ K}^{-1}$  (20-700°C) et une décoration sur la surface de ladite plaque, caractérisée en ce que ladite décoration comprend une fritte de verre vitrifiée :

20            - ladite fritte de verre a un coefficient de dilatation thermique de  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300°C), de préférence de  $30-35 \times 10^{-7} \text{ K}^{-1}$  (0-300°C) et un point de ramollissement d'au moins 750°C, de préférence d'au moins 775°C ;

25            - la composition de ladite fritte de verre, calculée en pourcentage massique d'oxydes, consiste essentiellement en 70-82 % de SiO<sub>2</sub>, 12-18 % de B<sub>2</sub>O<sub>3</sub>, 1-3 % de Al<sub>2</sub>O<sub>3</sub>, au plus 5% de Na<sub>2</sub>O + K<sub>2</sub>O et au plus 1,2 % d'au moins un agent affinant ; et

30            - ladite fritte de verre contient de 10 à 35 % en masse de pigments ;

35            et en ce que ladite plaque de vitrocéramique décorée présente un module de rupture d'au moins 120 MPa.

40            2. Plaque de vitrocéramique décorée selon la revendication 1, caractérisée en ce que le verre qui constitue ladite fritte est un borosilicate de sodium et de potassium.

45            3. Plaque de vitrocéramique décorée selon l'une des revendications 1 ou 2, caractérisée en ce que la composition de ladite fritte de verre consiste essentiellement en 76-81 % de SiO<sub>2</sub>, 14-15,5 % de B<sub>2</sub>O<sub>3</sub>, 2-2,7 % de Al<sub>2</sub>O<sub>3</sub>, 2,3-3,2 % de Na<sub>2</sub>O, 1-1,5 % de K<sub>2</sub>O et 0-1 % de As<sub>2</sub>O<sub>3</sub>, Sb<sub>2</sub>O<sub>3</sub>.

50            4. Plaque de vitrocéramique décorée selon l'une des revendications 1 à 3, caractérisée en ce que ladite plaque de vitrocéramique a un coefficient de dilatation thermique dans le domaine de  $0\pm3 \times 10^{-7} \text{ K}^{-1}$  (20-700°C).

55            5. Procédé de décoration d'une plaque de vitrocéramique, ladite plaque présentant un faible coefficient de dilatation thermique compris entre  $\pm 15 \times 10^{-7} \text{ K}^{-1}$  (20-700°C), caractérisé en ce qu'il comprend :

60            - la production d'un mélange de 65 à 90 % en masse d'une fritte de verre et de 10 à 35 % en masse de pigments, ladite fritte de verre présentant un coefficient de dilatation thermique de  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300°C), de préférence de  $30-35 \times 10^{-7} \text{ K}^{-1}$  (0-300°C) et un point de ramollissement d'au moins 750°C, de préférence d'au moins 775°C ; et la composition de ladite fritte de verre, calculée en pourcentage massique d'oxydes, consiste essentiellement en 70-82 % de SiO<sub>2</sub>, 12-18 % de B<sub>2</sub>O<sub>3</sub>, 1-3 % de Al<sub>2</sub>O<sub>3</sub>, au plus 5 % de Na<sub>2</sub>O + K<sub>2</sub>O et au plus 1,2 % d'au moins un agent affinant ;

65            - l'application dudit mélange fritte de verre/pigments sur la surface d'une plaque de vitrocéramique ou sur la surface d'une plaque de verre précurseur de vitrocéramique ;

70            - la cuisson de ladite plaque revêtue dudit mélange fritte de verre/pigments, pour éventuellement transformer ladite plaque de verre en plaque vitrocéramique, pour vitrifier la fritte de verre dans le mélange fritte/pigments, pour produire une adhérence de la décoration générée avec la vitrocéramique ; et

75            - le refroidissement de ladite plaque cuite pour obtenir une plaque de vitrocéramique décorée ayant un module de rupture d'au moins 120 MPa.

80            6. Procédé selon la revendication 5, caractérisé en ce qu'il comprend l'application dudit mélange fritte de verre/pigments sur la surface d'une plaque de vitrocéramique puis le traitement thermique dudit mélange fritte de verre/pigments pendant environ 15 min à une température dans le domaine de 920-960°C.

85            7. Procédé selon l'une des revendications 5 ou 6, caractérisé en ce qu'il comprend l'application dudit mélange fritte

de verre/pigments sur la surface d'une plaque vitrocéramique ayant un coefficient de dilatation thermique dans le domaine de  $0 \pm 3 \times 10^{-7} \text{ K}^{-1}$  (20-700°C).

5 8. Procédé selon la revendication 5, caractérisé en ce qu'il comprend l'application dudit mélange fritte de verre/pigments sur la surface d'une plaque de verre précurseur de vitrocéramique puis le traitement thermique de ladite plaque de verre précurseur et dudit mélange fritte de verre/pigments appliqués sur celle-ci, selon le programme suivant :

10 - augmentation de température à une vitesse de 50-80°C/min jusqu'au domaine de nucléation, généralement situé à proximité du domaine de transformation de verre,

- augmentation de température dans le domaine de nucléation (670-800°C) en environ 15-25 min,
- augmentation de température jusqu'à la température de cristallisation (900-960°C) en environ 15-30 min,
- maintien de la température de cristallisation pendant 10-25 min, et
- refroidissement rapide à la température ambiante.

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9. Email, notamment utile à la mise en œuvre du procédé selon l'une quelconque des revendications 5 à 8, caractérisé en ce qu'il comprend de 10 à 35 % en masse de pigments et de 85 à 90 % en masse d'une fritte de verre présentant un coefficient de dilatation thermique de  $30-40 \times 10^{-7} \text{ K}^{-1}$  (0-300°C), de préférence de  $30-35 \times 10^{-7} \text{ K}^{-1}$  (0-300°C) et un point de ramollissement d'au moins 750°C, de préférence d'au moins 775°C ; la composition de ladite fritte de verre, calculée en pourcentage massique d'oxydes, consistant essentiellement en 70-82 % de  $\text{SiO}_2$ , 12-18 % de  $\text{B}_2\text{O}_3$ , 1-3 % de  $\text{Al}_2\text{O}_3$ , au plus 5 % de  $\text{Na}_2\text{O} + \text{K}_2\text{O}$  et au plus 1,2 % d'au moins un agent affinant.

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10. Email selon la revendication 9 caractérisé en ce que la composition de ladite fritte de verre, calculée en pourcentage massique d'oxydes, consiste essentiellement en 76-81 % de  $\text{SiO}_2$ , 14-15,5 % de  $\text{B}_2\text{O}_3$ , 2-2,7 % de  $\text{Al}_2\text{O}_3$ , 2,3-3,2 % de  $\text{Na}_2\text{O}$ , 1-1,5 % de  $\text{K}_2\text{O}$  et 0-1 % de  $\text{As}_2\text{O}_3 + \text{Sb}_2\text{O}_3$ .

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